





2016 NIAC Phase I Study Journey to the Center of Icy Moons

# **Enceladus Vent Explorer Concept**

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Jet Propulsion Laboratory
California Institute of Technology

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### Enceladus Vent Explorer (EVE) Goals



- Pathfinder mission concept into Enceladus vent
- Characterize the interior environment of vent
- Assess the accessibility to the subsurface ocean through vent
- Perform astrobiology and volcanology observations in the vent
- Potentially reach the liquid interface/ocean



#### Talk Outline



- Mission Concept
- Characterization of Enceladus Vent Environment
- Trade Studies
- Planetary Protection
- Experimental Studies
- Mechanical Prototype Design



#### Talk Outline



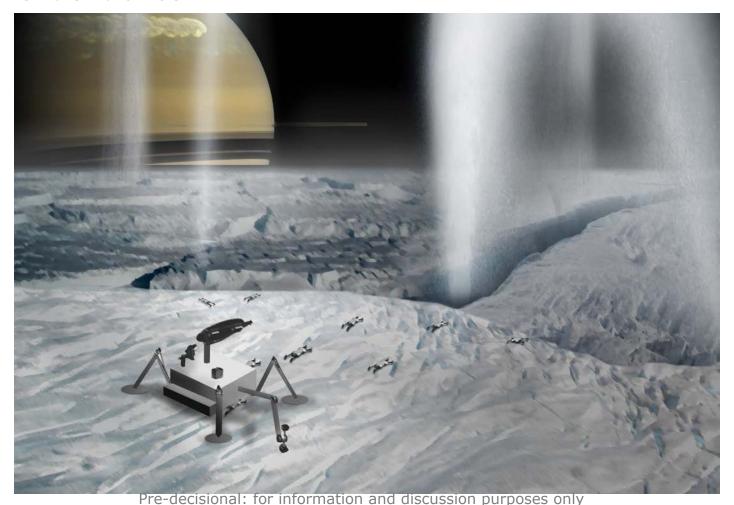
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#### EVE Concept - SM Landing and DM Deployment



- Surface module (SM) lands near the vent (within 100s of meters)
- Tens of descent modules (DMs) are released from SM and move to the vent entrance

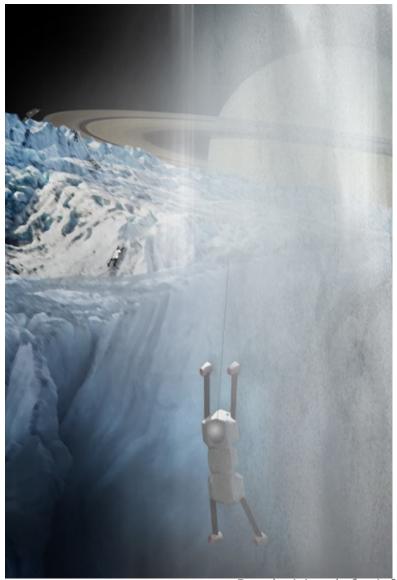




### EVE Concept - Journey into the Vent



#### Force from upward flow >> gravity (0.01g)



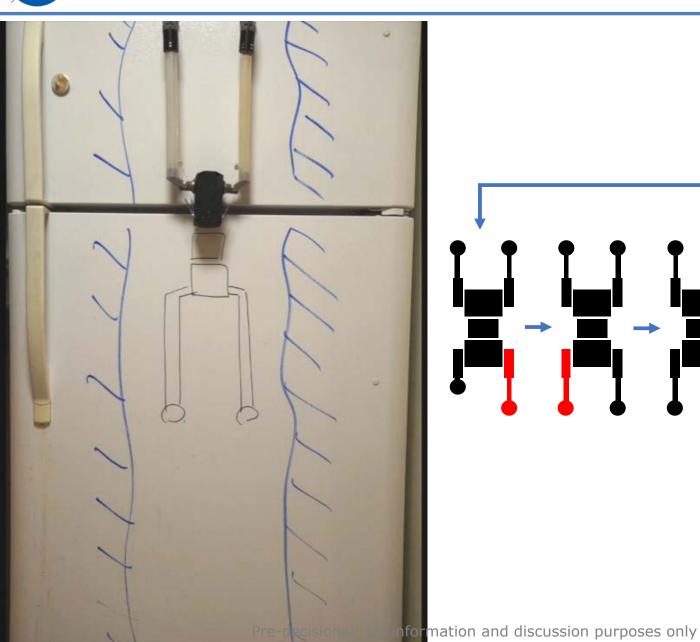
Ice screw end effector-**Linear joint** Rear section (mobility, tether spool) **Instrument section** Front section (mobility, stereo camera) Mass: ~3 kg Estimated speed: 5.5 m/hr ~10cm @ 10<sup>5</sup> Pa, 10W SM supports power & comm via 6

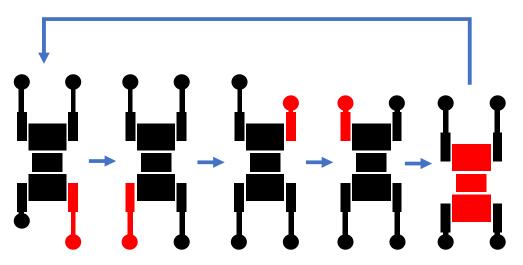
cable Pre-decisional: for information and discussion purposes only



### **DM** Gait





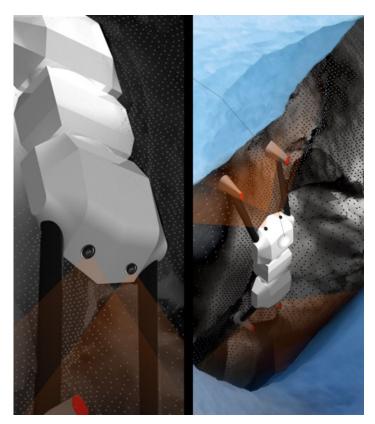




### EVE Concept - Scout/In-situ Science DMs



#### **Scout DMs**



3D mapping of vent using structured light + stereo camera

#### **In-situ science DMs**



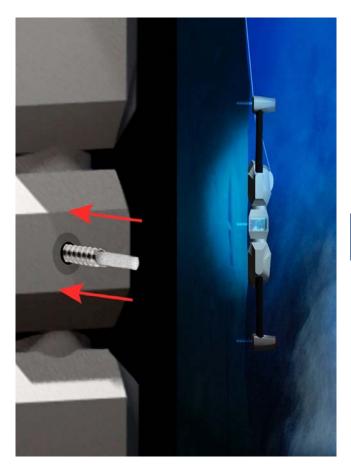
- Astrobiology/volcanology observations by a heterogeneous team of DMs
- One instrument per DM due to



### EVE Concept - Sample Return DMs



- Collect ice cores/particles in the vent
- Return to SM for detailed analysis (e.g., mass spectrometer)
- One ice core per DM per trip for mechanical simplicity









### **EVE Concept - SM**





- Used Europa Lander concept's design as a reference
- Europa Lander:
  - 100 m landing accuracy
  - 45 kWh primary battery (~95kg)
  - 42.5 kg payload
  - 20-day mission
  - 5 ice samples
- EVE SM
  - Baseline power system uses
     RTG
    - MMRTG: 45 kg, 125W at start, 100W after 14 yrs
  - ~10 DMs + science instruments



#### Talk Outline



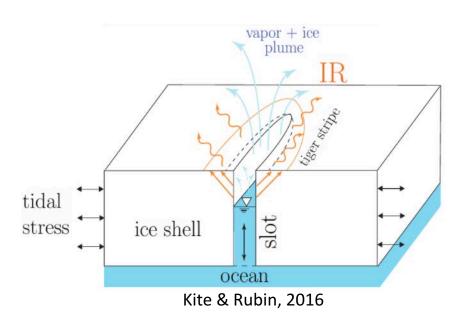
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### **Eruption Models**

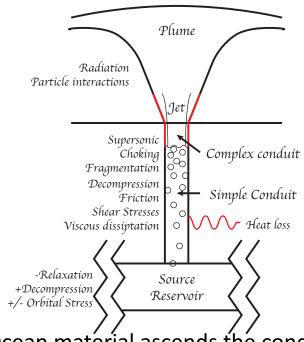


#### "Boiling" model



 Liquid water boils into vapor under the surface

#### "Cryovolcanic" model



Ocean matérial ascends the conduit driven by exsolution and expansion of dissolved materials and phase changes

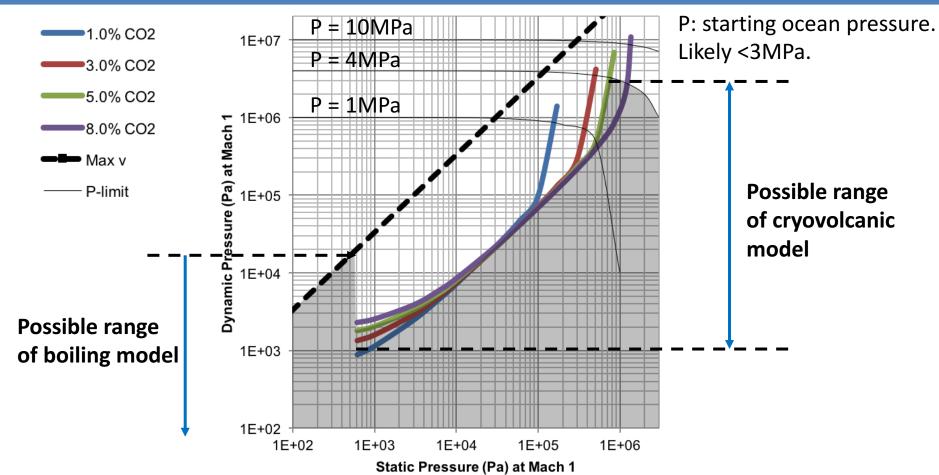
|                                 | Boiling model       | Cryovolcanic model                   |
|---------------------------------|---------------------|--------------------------------------|
| Dynamic pressure of upward flow | <10 <sup>4</sup> Pa | 10 <sup>3</sup> – 10 <sup>7</sup> Pa |
| Vent width                      | <1 m                | 1 – 30 cm                            |
| Feasibility of EVE              | Likely feasible     | Undetermined 12                      |

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### **Dynamic Pressure Modeling**





#### Major Assumptions

- Most of the acceleration occurs in the subsurface
- Water erupts at sub-triple points pressures
- CO2 as a proxy for all non-water volatiles (not as the driving mechanism of eruption)
- Flow chokes (=Mach 1) at or near the surface
   Pre-decisional: for information and discussion purposes only
   Work by Karl Mitchell



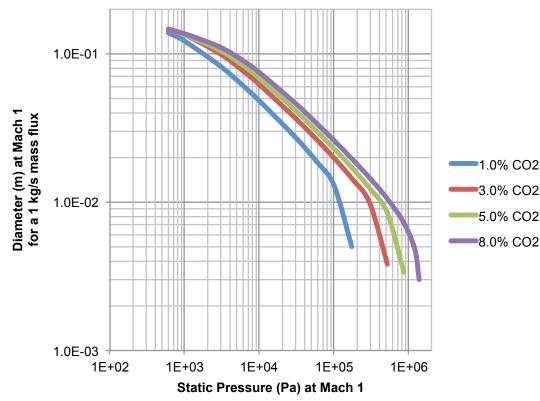
### Vent Size Modeling



#### Boiling model:

- 2.5-m fissure with a very low eruption density (Kite and Rubin, 2017)
- Cryovolcanic model
  - 1-30 cm width
  - Likely evolve towards pipe-like structures
    - Driver towards the small end
  - Greater mass flux results in greater size
    - EVE would target at vent with greatest mass flux

### Vent size estimate for 1 kg/s cryovolcanic vent (diameter @ choking point)





#### Talk Outline

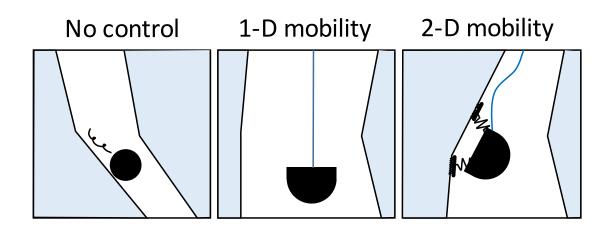


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### Mobility





- Even with the most optimistic estimation of dynamic pressure (10<sup>3</sup> Pa), the upward force from flow is an order of magnitude stronger than gravity (0.01g)
  - Assumed a sphere with 5cm radius, 2000kg/m³ density
  - 0.24N from gravity, 1.9N from flow
  - Needs ~80 cm radius for free-fall greater than the most optimistic estimation of vent width
- Conclusion: 2-D mobility (active descent) would be required for EVE



### **Attachment Mechanism Options**



#### **Ice Screw**





Archemedes screw

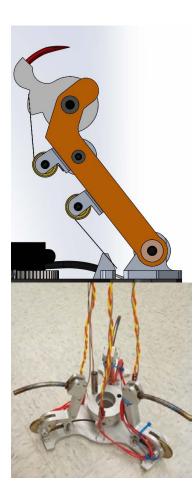
Melt anchor













Single Wall Capable

>4 Actuators required for movement (Assumes limbed muti DOF)

### Attachment Mechanism Trade Study



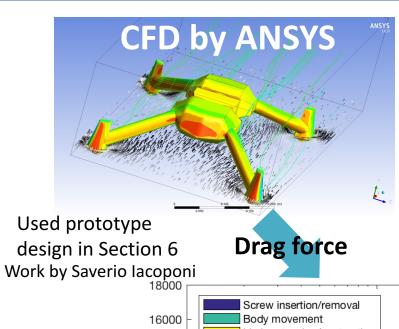
#### **Pugh Matrix**

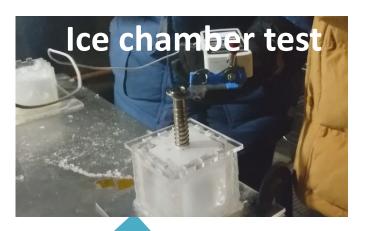
| I agri Matrix   |                  |                          |                               |                                 |                           |                                    |            |  |
|---|------------------|--------------------------|-------------------------------|---------------------------------|---------------------------|------------------------------------|------------|--|
| Design  | Factor<br>Weight | Dynamic<br>Pressure<br>5 | Properties of<br>the Ice<br>5 | Geometry of<br>the Conduit<br>5 | Surface<br>Roughness<br>5 | Energy/Resou<br>rces Required<br>5 | Totals     |  |
| Ice Screw   |                  | 8                        | 7                             | 10                              | 9                         | 4                                  | 190        |  |
| Microspine<br>Gripper                                 |                  | 6                        | 3                             | 10                              | 2                         | 6                                  | 135        |  |
| Cam/Wedging   |                  | 7                        | 5                             | 5                               | 7                         | 7                                  | 155        |  |
| Archimedes<br>Screw                                   |                  | 8                        | 6                             | 6                               | 8                         | 8                                  | 180        |  |
| Melt Anchors  |                  | 8                        | 7                             | 10                              | 9                         | 3                                  | 185        |  |
| Rank each desig<br>of each aspect.<br>Hollow Interior | n in each        | category. 1 is th        | ne worst, 10 is               | the best. The v                 | weights determ            | ine the relative                   | importance |  |
| Penetrates Ice  |                  |                          |                               |                                 |                           |                                    |            |  |

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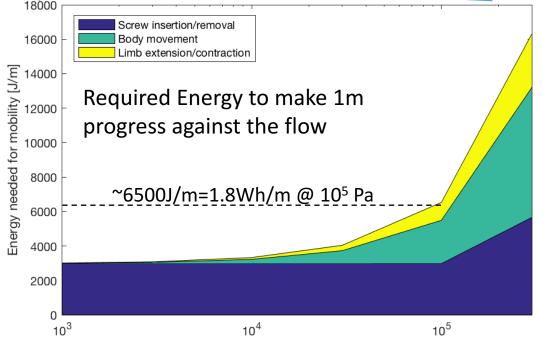
### Power System: Estimation of Required Energy





#### **Energy for screwing in/out**

Work by Ellie Simonson, Saverio Iacoponi, Aaron Curtis

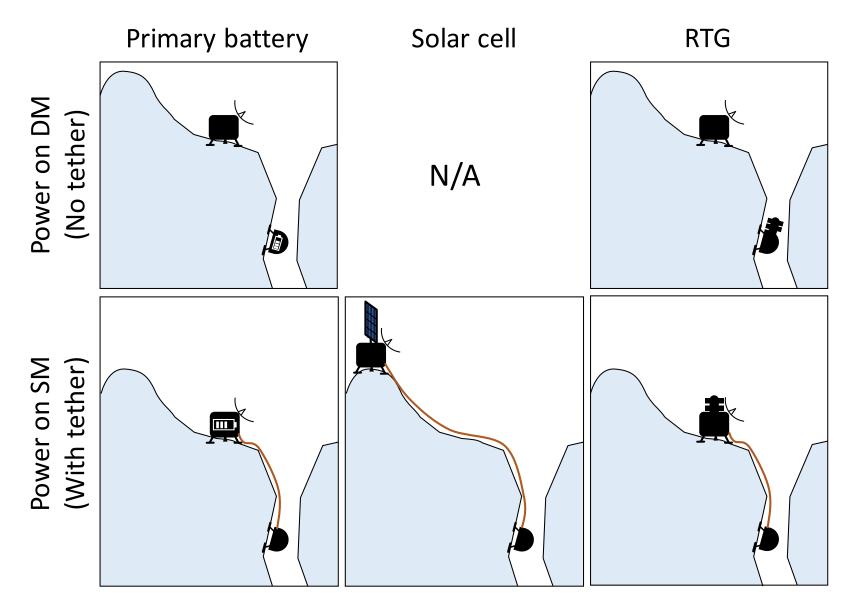


Estimated speed: 5.5 m/hr @ 10<sup>5</sup> Pa (Assumed 10W for mobility)



### **Power Options Study**







### Power System Trade



- RTG on SM would be most viable
- Power on DM would not be realistic
- Primary battery/solar cell on SM would be possible but

| Configuration              | Energy<br>source   | Distance<br>(m)               | Speed<br>(m/hr) | Max<br># of<br>DMs | Major risk  |
|----------------------------|--------------------|-------------------------------|-----------------|--------------------|---|
| Power on DM<br>(No tether) | Primary<br>battery | 350                           | 5.5             | 10                 | Unreliable comm.  |
|                            | RTG                | 1300 (per<br>year)            | 0.15            | 10                 | Unreliable comm.  |
| Power on SM (With tether)  | Primary<br>battery | 2600 (all<br>DMs<br>combined) | 5.5             | 1-3                |   |
|                            | Solar cell         |                               | 5.5             | 1-2                | Needs at least 20 m <sup>2</sup> solar cell; Landing site constrained by sunshine |
|                            | RTG                |                               | 5.5             | >10                |   |

Assumed 10W for DM mobility. The distance of "power on DM" configurations is the distance that can be traveled by <u>each</u> DM, while that of "primary battery on SM" is the total distance traveled by all DMs combined. The distance of "power on DM"-RTG is bounded not by available energy but by mission duration due to its slow speed. Max number of DMs of "power on DM" configurations is bounded by the payload mass of SM, while that of "power on SM" configurations is bounded by power, hence it represents the number of DMs that can be operated simultaneously. (SM can bring more DMs.)

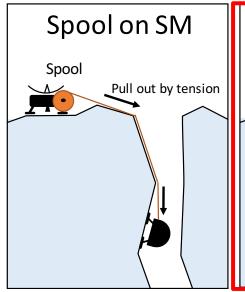
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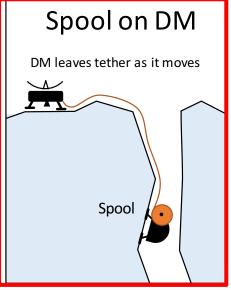


### **Tether System Trade**



#### **Tether system options**







38 AWG magnet wire (d=0.101mm)

Assumption: Tether consists of three 38 AWG wires (GND, PWR, DATA)

- Spool on SM
  - DM needs to pull out by tension
  - Need to support mechanical strength
  - Abrasion is another challenge
- Spool on DM
  - No tension needed for deployment
  - No abrasion
  - Range limited by tether length
- Tether volume/mass/resistance
  - 2km tether: 48 cm<sup>3</sup>, ~0.4kg, 600Ω
  - 10km tether: 240 cm<sup>3</sup>, ~2kg, 3k $\Omega$
- 2 km tether is feasible for the standard three-section DM design
- 10 km tether possible with a dedicated tether section on DM

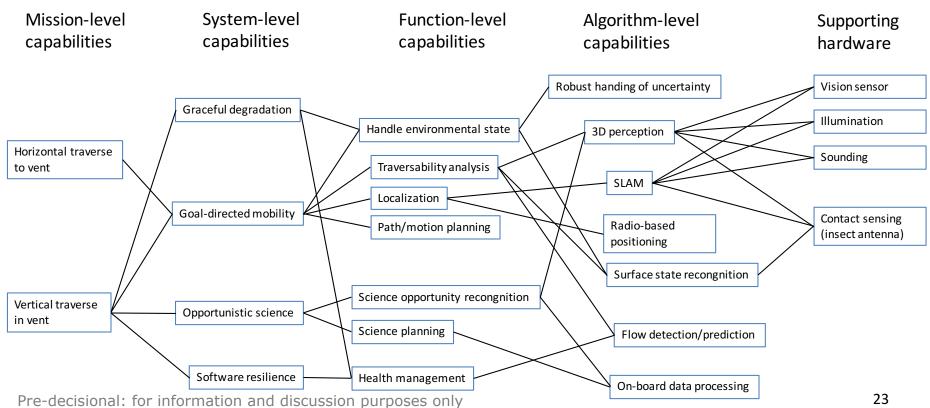


### **Autonomy System**



- High-level automation is needed for DM due to:
  - Unavailability of orbital reconnaissance prior strategic planning impossible
  - Poor viewshed tens of cm progress per planning cycle if manually operated
  - Multiplicity of DMs operation tens of DM manually increases cost/labor
  - Dynamic environment need immediate response to anomalies

#### **Autonomy Capability Roadmap**

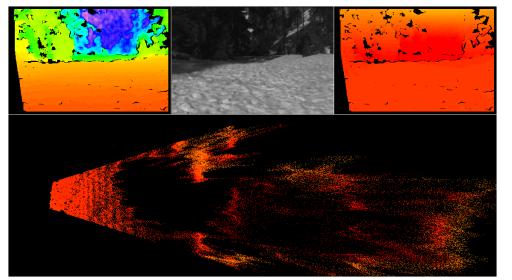




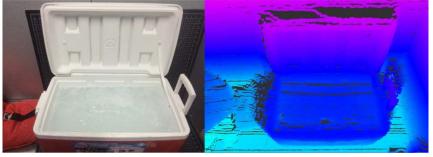
### Perception System: Options



#### **Stereo vision**

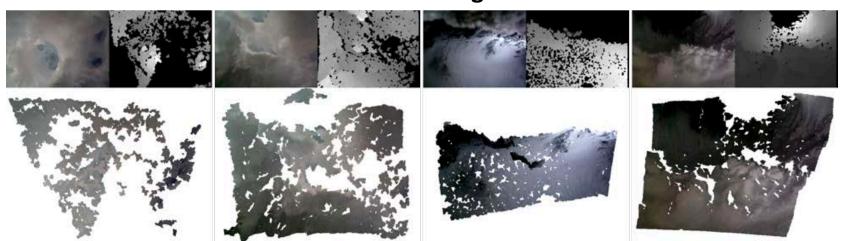


#### **Spinning Lider**



Other options: ToF camera, Rader

#### **Structured light**



depth: 70cm

depth: 90cm depth: 2m
Pre-decisional: for information and discussion purposes only
Work by Renaud Detry/Jeremy Nash

depth: 5m



### Perception System Trade



|                                 | Powe<br>Cons | er<br>umption           | Dev<br>Volu |                     |   | Sensing Sensing Accuracy                      |   |  | Temperature<br>Resistance |                         |
|---------------------------------|--------------|-------------------------|-------------|---------------------|---|---|---|--|---------------------------|-------------------------|
| Stereo<br>Vision                | 3            | 5W exposure: .1s-inf    | 4           | 2x1cm <sup>3</sup>  | 4 | 0.1m-inf (further with longer exposure)       | 2 | Fails if no texture                          | 3                         |                         |
| Structured<br>Light             | 3            | 7.5W exposure: .1s–inf  | 4           | 2x1 cm <sup>3</sup> | 4 | 0.1m-inf<br>(further with longer<br>exposure) | 3 |  | 3                         |                         |
| Stereo +<br>structured<br>light | 3            | 7.5W exposure: .1s–inf  | 3           | 3x1 cm <sup>3</sup> | 4 | 0.1m-inf<br>(further with longer<br>exposure) | 3 | Superior<br>to stereo or<br>structured light | 3                         |                         |
| ToF<br>Camera                   | 4            | >10W<br>exposure: flash | 2           | 100 cm <sup>3</sup> | 2 | 0.1m-10m                                      | 4 |  | 3                         |                         |
| Spinning<br>Lidar               | 1            | 10W scan:<br>5s         | 1           | 100 cm <sup>3</sup> | 3 | 0.1m-30m                                      | 4 |  | 1                         | mechanical sensitivity? |
| Radar                           | ≤3           | >5W                     | ≤2          | <4 cm <sup>3</sup>  | 4 | ~100m   | 0 | Beam width >1° range accuracy >25cm          | 3                         |                         |

### Science Instrument Options for In-Situ Discrete

- Volcanology package: temperature, pressure, flow speed
  - Vent environment & eruption mechanism
- Habitability package: pH, salinity, and oxidation-reduction potential (ORP)
  - Habitability of vent & ocean
- Microscopic imager
  - Detecting patterns indicating life
- Life detection package: microchip electrophoresis with laser-induced fluorescence
  - Detect the distribution of organics that is characteristic to life
- Each DM carries one of above



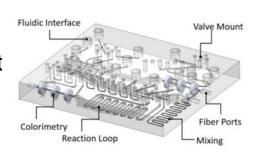
← Miniature pH probe (Kehl, et al., 2016)

MSL's Mars Hand Lens Imager (MAHLI)→





Macroscopic (left) and microscopic (right) patterns indicating life. (Jones, et al., 2008) (Boston, et al., 2001)





An example of microfluidics chip. Left: 3D printed MicroFIA manifold, right: assembled MicroFIA system. Images taken from (Kehl, et al., 2016)

Based on inputs from Peter Willis, Florian Kehl, Penny Boston, Karl Mitchell

Pre-decisional: for information and discussion purposes only



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### Planetary Protection Considerations



- Enceladus is a Category III/IV body in COSPAR/NASA PP policy (NPR 8020.12D)
- "The probability of inadvertent contamination of an ocean or other liquid water body" must be reduced to less than  $1\times10^{-4}$  per mission (NPR 8020.12D, Sec. 5.4).
- DM could directly contact the liquid body of water; significantly more elaborate bioburden reduction processing would be necessary than landing missions
- A similar level of bioburden reduction processing would be necessary for SM because
  - DMs would be in contact with SM over a long period
  - Upon a failed landing or spacecraft disintegration, SM's RTGs (baseline power system) could melt through the ice shell and reach the subsurface ocean
- Common misconception: RTG is prohibited for icy worlds
  - There is no such rules in COSPAR/NASA's PP policy. However, increased level of bioburden reduction would be needed to achieve the  $1\times10^{-4}$  contamination probability requirement as RTG could melt through the ice and reach a subsurface ocean over a long period.



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## mergy Required for Ice Screw Insertion/Removale

- Ice screw is intended for manual operation; no info on needed energy on the catalog specs
- Experiment:
  - Used −20°C chamber at JPL
  - Black Diamon's ice screw; 100 mm in length, 19.5 mm in diameter
  - Insertion depth: 72mm
- Result: ~500 J for insertion AND removal
- Extrapolation for ice screws with different sizes
  - Assumption: energy scales with (screw diameter)x(insertion depth)



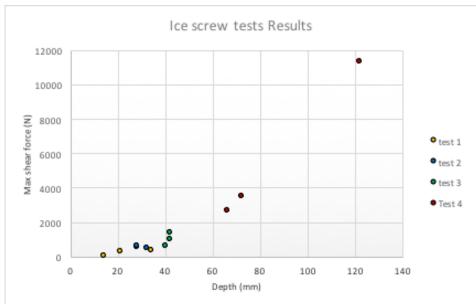


### Ice screw's resistance to shear force



- **Experiment setup** 
  - Used a pressing stand with max load of 40 klbs at JPL
  - Black Diamon's ice screw; 100 mm in length, 19.5 mm in diameter
  - Manufactured ice container with screw attachment made of Al 7075 T3
  - Made ice in a cold chamber at -10°C.
  - Insert a screw horizontally; press the screw downwards until ice breaks
  - Measure the max load
- Results were used to estimate the necessary screw insertion depth for a given drag force exerted on DM

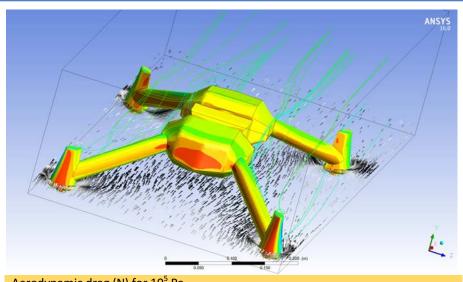




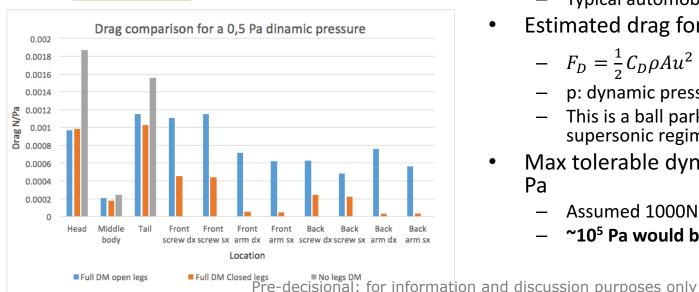


#### CFD Analysis of Aerodynamic Drag





| Aerodynamic drag (N) for 10 <sup>5</sup> Pa |            |              |          |
|---|------------|--------------|----------|
| dynamic pressure                            | Open limbs | Closed limbs | No limbs |
| Total Body + Legs                           | 1671       | 744          |          |
| Total Body                                  | 466        | 437          | 734      |



- Purpose: estimate the drag coefficient (C<sub>D</sub>)
- Used the prototype design (detailed in next section) with three configurations:
  - Open limbs
  - Closed limbs
  - No limbs
- Imposed a fixed dynamic pressure of 0.5 Pa
  - k-ε model with an inlet speed of 1 m/s and a turbulence of 5%
- Result (closed limb):  $C_D A \sim 7.5 \times$  $10^{-3}$  m<sup>2</sup>,  $C_D \sim 1.5$ 
  - Design optimization could reduce C<sub>D</sub> significantly
  - Typical automobile:  $C_D = 0.2 0.3$
- Estimated drag force by:

$$-F_D = \frac{1}{2}C_D \rho A u^2 = C_D A p$$

- p: dynamic pressure
  - This is a ball park as flow behaves differently in supersonic regime
- Max tolerable dynamic pressure: 5.4x10<sup>5</sup> Pa
  - Assumed 1000N limit for each limb
  - ~10<sup>5</sup> Pa would be the safe operational limit



#### Talk Outline



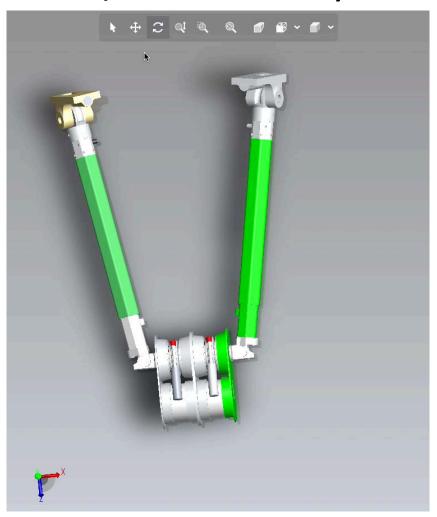
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#### Overview



#### Head/tail section assembly

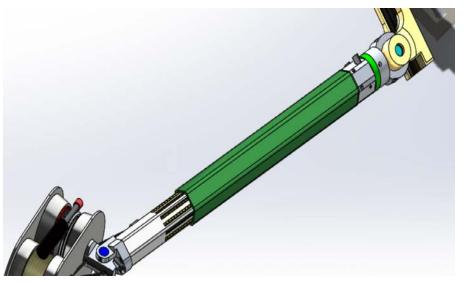


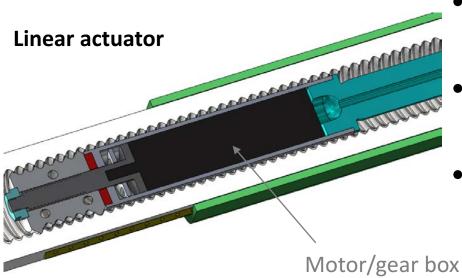
- A point design, not the optimal one, to serve as a reference point for system trade study
  - Gives conservative estimation of drag force (through CFD), size, mass
  - In particular aerodynamic design could be significantly improved
- Only used existing technologies and commercially available mechanical parts (e.g., motors, gear boxes)
- 5DOF per limb
  - 1 DOF linear joint
  - 2 DOF at shoulder
  - 2 DOF at wrist



### Linear Actuator Design





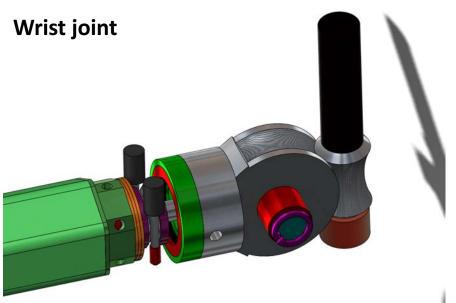


- Features a linear actuator
  - Only the linear actuator need to work against the flow
  - Can keep "closed limb" formation to minimize aerodynamic drag
- Uses conventional electromechanical actuators
- Designed to support 1000
   N of force per limb
- Ball bearing with recirculating balls



### Joint Design

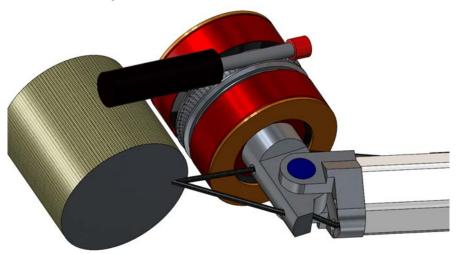




Section of wrist joint

- Wrist joints are actuated by worm gears and motors
- Shoulder joints are actuated by worm gears and tendon actuator
- Shoulder actuators are housed in the head/tail section body

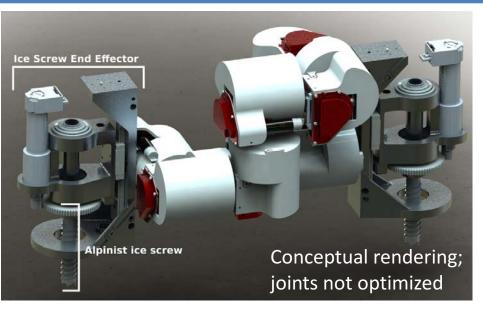
#### **Shoulder joint actuators**



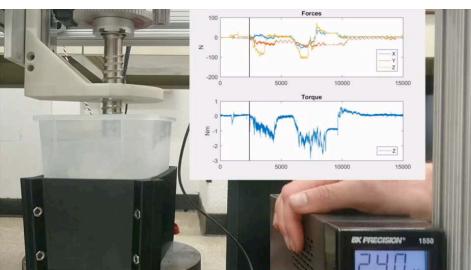


### Ice Screw End Effector (ISEE)





- Designed for LEMUR
  - ~10x10x10 cm in size
  - Need to be miniaturized for EVE
- Prototype tested in ice chamber to measure required normal force/torque
- Field test in Helo Cave on Erebus volcano in Antarctica







#### **Future Work**



- Resolve between boiling and cryovolcanic models
  - Probably require observations by ELF
  - Refinement of dynamic pressure/vent size estimates is possible with additional studies of *Cassini* data
- Optimization of DM design
  - Improvement of drag coefficient  $C_D$ =1.5 is too high
  - Improve strength of linear actuator
  - Explore alternative DM designs (e.g., snakebot)
- Development of required autonomy capabilities
  - Resilience/goal-directed mobility/graceful degradation/etc
- System trade study of SM, carrier-relay orbiter, and SM-DM interface
- Explore Advanced ideas
  - Interchangeable instrument section
- Consider Europa/terrestrial applications



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### Behind the Scenes...





